

# 即時控制系統設計

## Design of Real-Time Control Systems

### Lecture 25

#### Techniques for Enhancing the Performance of Discretized Controllers

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Feb10 – Jun10

Figures and images used in these lecture notes are adopted from

1: B.D.O. Anderson, "Controller Design: Moving from Theory to Practice," IEEE Control Systems Magazine, 13(4), pp. 16-25, Aug. 1993

2: D. Raviv &amp; E.W. Djaja, "Technique for Enhancing the Performance of Discretized Controllers," IEEE Control Systems Magazine, 19(3), pp. 52-57, June 1999

### Digital Control Systems

#### ▪ Study in Digital Control Systems

- Controller Design of Digital Control Systems
  - Design Process

##### > Emulation:

- » CT plant  $\rightarrow$  CT controller  $\rightarrow$  DT controller

##### > Discrete Design:

- » CT plant  $\rightarrow$  DT plant  $\rightarrow$  DT controller

##### > Direct Design: (B.D.O. Anderson, 1992 Bode Prize Lecture)

- » CT plant  $\rightarrow$  DT controller

### Basic Design Concept

#### ▪ Basic principles of low-order controller design

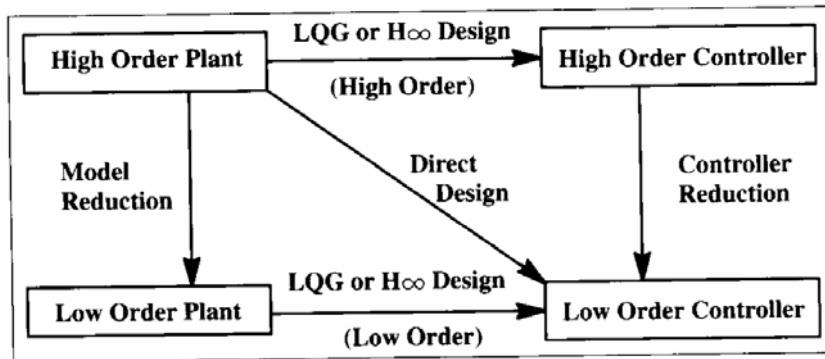


Fig. 1. Basic principles of low order controller design.

Anderson 1993

### Basic Design Concept

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NTUEE-RTCS25-DiscretizedCtrl-4

#### ▪ Textbook schemes for replacing a CT controller by a DT one

With  $C(s)$  continuous time and  $C_d(z)$  discrete time,

$$C_d(z) = C \left( \frac{z-1}{T} \right)$$

Euler or forward difference

$$C_d(z) = C \left( \frac{z-1}{zT} \right)$$

Balanced difference

$$C_d(z) = C \left( \frac{2z-1}{Tz+1} \right)$$

Tustin or bilinear

$$C_d(z) = C \left( \tan \left( \frac{\omega_1 T}{2} \right) \frac{z-1}{Z+1} \right)$$

Tustin with prewarping

$$C_d(z) = \frac{(z-1)}{Tz} \frac{1}{2\pi j} \int_{\gamma-j\infty}^{\gamma+j\infty} \frac{e^{sT}}{z-e^{sT}} \frac{G(s)}{s} ds$$

Step-invariance

$$C_d(z) = \frac{(z-1)^2}{Tz} \frac{1}{2\pi j} \int_{\gamma-j\infty}^{\gamma+j\infty} \frac{e^{sT}}{z-e^{sT}} \frac{G(s)}{s^2} ds$$

Ramp-invariance

Poles and zeros of  $C_d(z)$  are images under  $z = e^{j\omega T}$  of those of  $C(s)$ , with  $C_d(1) = C(0)$ .Zero-order hold equivalence.  
First-order hold equivalence.  
Triangular-hold equivalence.

Anderson 1993

## Problem Formulation

- Digital control design through discretizing an analog controller

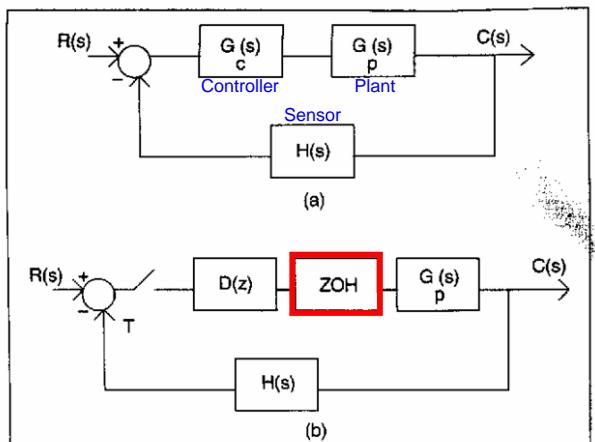


Fig. 1. (a) The analog closed-loop control system, (b) The digital closed-loop control system.

Raviv & Djaja 1999

## Problem Formulation

- Given

- A process  $G_p(s)$
- A sensor  $H(s)$
- A presumably well designed analog controller  $G_c(s)$

- Find

- A digital controller  $D(z)$   
which produces closed-loop behavior similar to the analog system both in the time and frequency domains

Raviv & Djaja 1999

## Problem Formulation

- Solutions:

- Analog control design followed by controller discretization
  - More convenient
  - Deal with sampling time  $T$  at the final phase
- Direct digital control design
- To enhance the performance by the first method
  - Add a pole-zero pair in the z-plane
  - To compensate for the low-frequencies and mid-frequencies phase and gain response effects contributed by ZOH

Raviv & Djaja 1999

## Problem Formulation

- Potential problem:

- The ZOH causes a delay of approximately  $T/2$

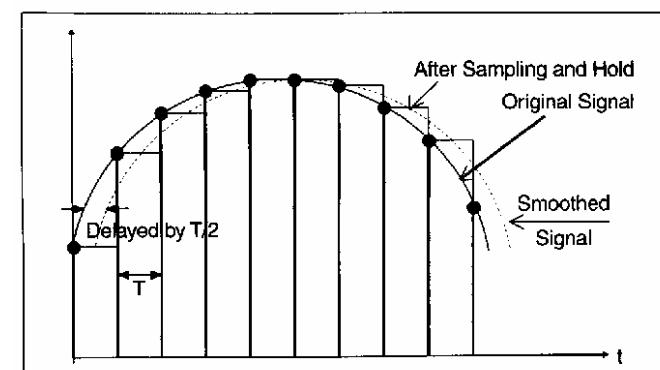


Fig. 2. A reconstructed signal using ZOH and its smoothed approximation.

Raviv & Djaja 1999

▪ A pole-zero compensation for delay:

$$C(z) = \frac{2z}{z+1}$$

- Provides a phase of  $(\omega T/2)$
- Which exactly cancels the frequency phase response of the ZOH obtained from

$$\frac{1 - e^{-sT}}{s}$$

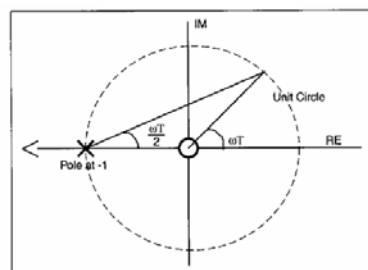


Fig. 3. The location of pole and zero of ZOH compensator in the Z-domain.

Raviv &amp; Djaja 1999

▪ A pole-zero compensation for delay:

- The ZOH transfer function:

$$\frac{1 - e^{-sT}}{s} \approx \frac{T}{1 + \frac{sT}{2}}$$

$$\Rightarrow \left. \frac{T}{1 + \frac{sT}{2}} \right|_{s=\frac{2}{T} \frac{z-1}{z+1}} = \frac{T}{2} \frac{z+1}{z}$$

1st-order Pade approximation

Tustin transformation

- The characteristic polynomial

$$1 + \left( \frac{2z}{z+1} \right) D'(z) (1 - z^{-1}) \mathcal{Z} \left\{ \frac{G_p(s)}{s} \right\} = 0$$

Raviv &amp; Djaja 1999

▪ A pole-zero compensation for delay:

- IF the proposed compensation causes instability a modified ZOH compensation

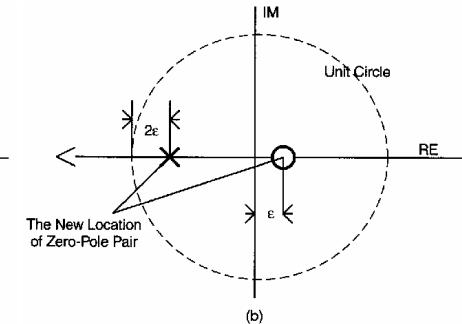
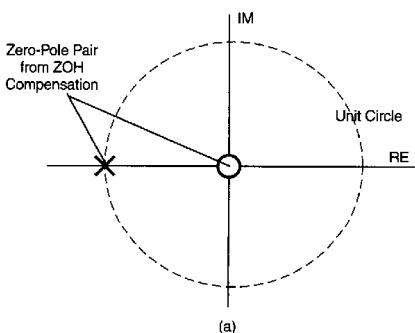
$$C'(z) = \frac{2(z-\varepsilon)}{z+1-2\varepsilon}$$

- The characteristic polynomial

$$1 + \left( \frac{2(z-\varepsilon)}{z+1-2\varepsilon} \right) D'(z) (1 - z^{-1}) \mathcal{Z} \left\{ \frac{G_p(s)}{s} \right\} = 0$$

Raviv &amp; Djaja 1999

▪ A pole-zero compensation for delay:



Raviv &amp; Djaja 1999

## Examples

### Lag Compensator:

$$G_p(s) = \frac{4 \times 10^6}{s(s+20)(s+200)}$$

$$H(s) = 1$$

- Design specifications:

- Velocity error constant  $K_v$  at least  $1000 \text{ s}^{-1}$
- Attenuation of all sinusoidal inputs of frequency above  $400 \text{ rad/sec}$  by at least 16
- Steady-state error of (up to) 1% for sinusoidal inputs for frequencies less than  $1 \text{ rad/sec}$

Raviv & Djaja 1999

## Examples

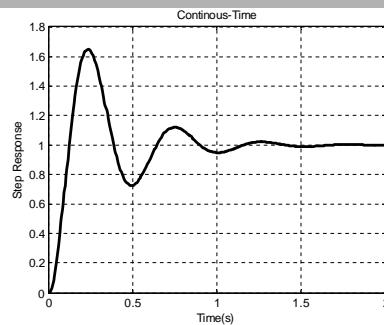
$$\Rightarrow G_c(s) = \frac{1}{80} \frac{(s+8)}{(s+0.1)}$$

Table 1

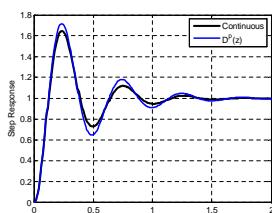
	$D'(z)$	Multiplier	$D(z)$
$T = 0.01 \text{ s}$	$\frac{0.0130z - 0.0120}{z - 0.9990}$	$\frac{2z}{z+1}$	$\frac{0.0260z^2 - 0.0240z}{z^2 + 0.0010z - 0.9990}$
$T = 0.05 \text{ s}$	$\frac{0.0150z - 0.0100}{z - 0.9950}$	$\frac{2z}{z+1}$	$\frac{0.0299z^2 - 0.0200z}{z^2 + 0.0050z - 0.9950}$
$T = 0.1 \text{ s}$	Unstable $0.0174z - 0.0075$ $z - 0.9900$	$\frac{2z}{z+1}$	Unstable $0.0348z^2 - 0.0150z$ $z^2 + 0.0100z - 0.9900$
$T = 0.1 \text{ s}$	Unstable $0.0174z - 0.0075$ $z - 0.9900$	$\frac{2(z-0.2)}{(z+0.6)}$	$0.0348z^2 - 0.0219z + 0.0030$ $z^2 - 0.3900z - 0.5940$

Raviv & Djaja 1999

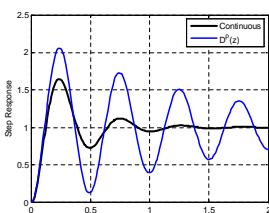
## Examples



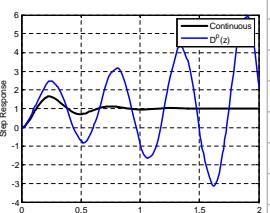
$T = 0.01 \text{ s}$



$T = 0.1 \text{ s}$

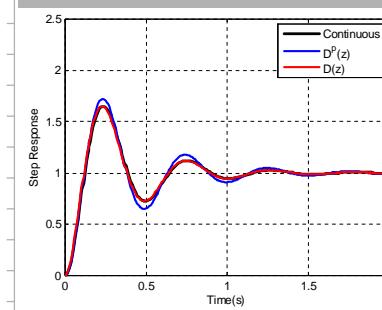


$T = 0.05 \text{ s}$

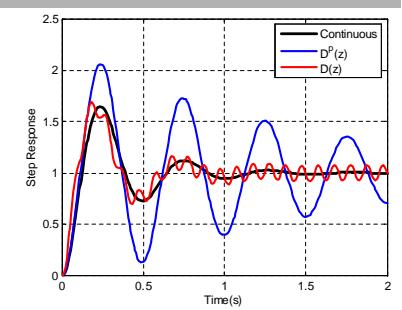


Raviv & Djaja 1999

## Examples

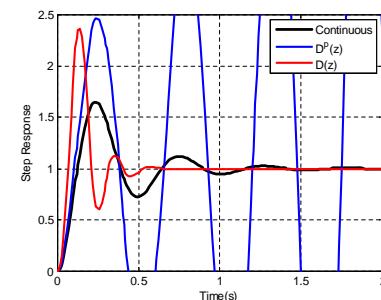


$T = 0.01 \text{ s}$



$T = 0.05 \text{ s}$

$T = 0.1 \text{ s}$



Raviv & Djaja 1999

## Examples

### ▪ Lead-Lag Compensator:

$$G_p(s) = \frac{1000}{s(1 + \frac{s}{10})(1 + \frac{s}{250})}$$

$$H(s) = 1$$

- Design specifications:

1. Phase margin of at least  $50^\circ$
2. Velocity error constant  $K_v$  at least  $1000 \text{ s}^{-1}$
3. Attenuation of the input noise at 60 Hz and above by a factor of 100
4. Steady-state error for frequencies less than 1 rad/sec less than 1%

Raviv & Djaja 1999

## Examples

$$\Rightarrow G_c(s) = \frac{(1 + \frac{s}{4.5})(1 + \frac{s}{10})}{(1 + \frac{s}{0.1})(1 + \frac{s}{110})}$$

$$T = 0.01s$$

$$\Rightarrow D'(z) = \frac{0.6597z^2 - 1.2897z + 0.6300}{1.00z^2 - 1.2893z + 0.2900}$$

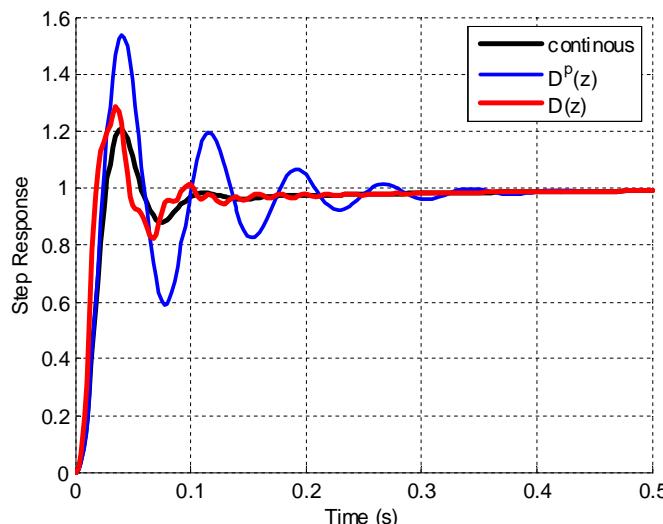


With the ZOH compensation of  $\frac{2z}{z+1}$

$$\Rightarrow D(z) = \frac{1.3194z^3 - 2.5793z^2 + 1.26z}{z^3 - 0.2893z^2 - 0.9993z + 0.2900}$$

Raviv & Djaja 1999

## Examples



Raviv & Djaja 1999



## Examples

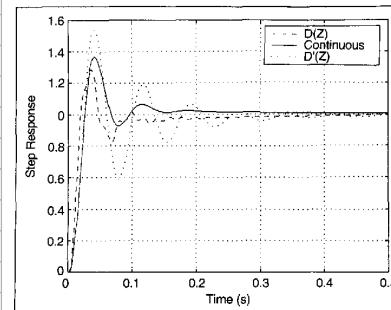
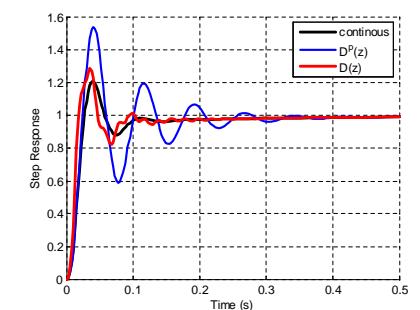
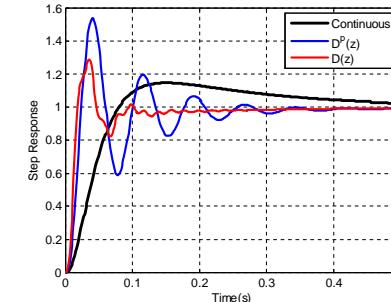


Fig. 6. Closed-loop step response of Example (b).  $T = 0.01 \text{ s}$ .



Raviv & Djaja 1999



## Examples

### Katz's Example:

$$G_p(s) = \frac{863.3}{s^2}$$

- Design specifications:

- Max phase lag at  $f = 3$  Hz should not be more than  $13^\circ$
- At any given frequency the CL gain should not exceed 5 dB beyond the CL dc gain
- Max tracking error due to an input disturbance moment of 0.028Nm should not be 0.01 rad

Raviv & Djaja 1999

## Examples

$$G_c(s) = 2940 \frac{(s + 29.4)}{(s + 294)^2}$$

$$T = 0.03s$$

$$\Rightarrow D'(z) = \frac{1.8958z^2 + 1.1685z - 0.7273}{z^2 + 1.1653z + 0.3395}$$

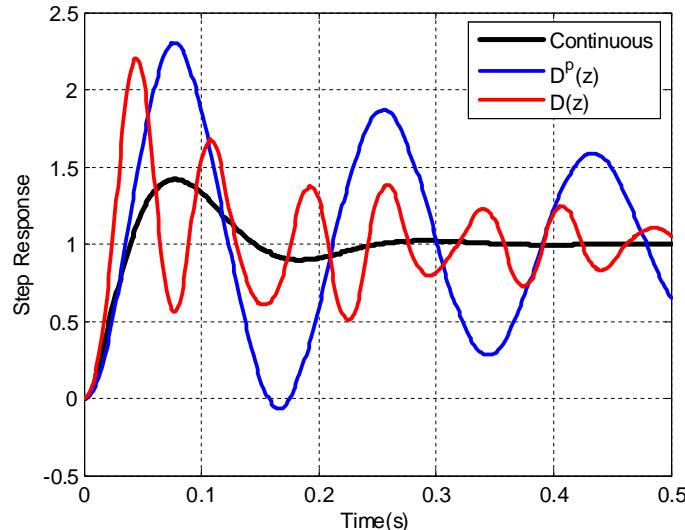
With the ZOH compensation of  $\frac{2z}{z+1}$

$$\Rightarrow D(z) = \frac{3.7916z^3 + 2.3369z^2 - 1.4546z}{z^3 + 2.1653z^2 + 1.5047z + 0.3395}$$

Raviv & Djaja 1999

## Examples

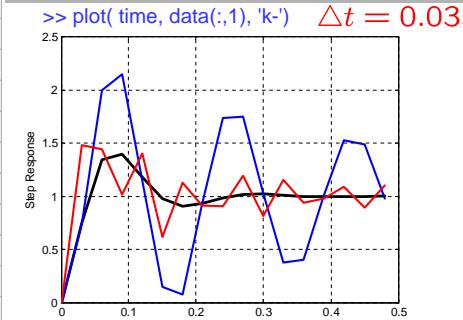
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Raviv & Djaja 1999

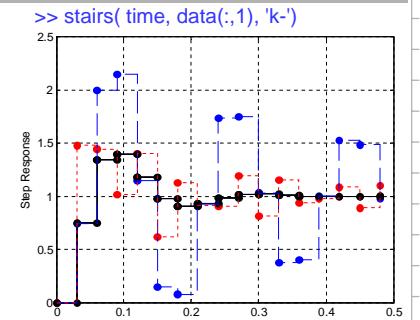
## Examples

$$T = 0.03s$$

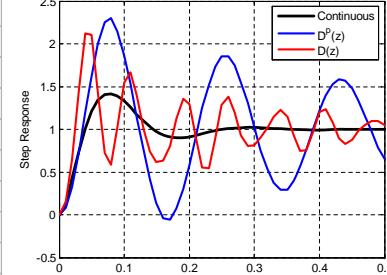


$$\Delta t = 0.03s$$

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$$\Delta t = 0.01s$$

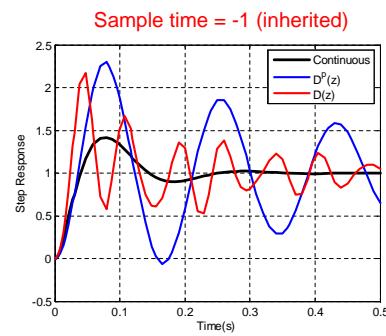
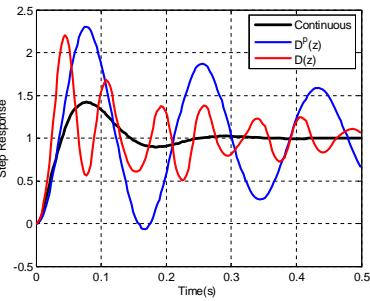


Raviv & Djaja 1999

## Examples

$T = 0.03s$

$\Delta t = 0.003s$



Raviv & Djaja 1999

## Examples

### Rattan's Example:

$$G_p(s) = \frac{10}{s(s+1)}$$

$$\Rightarrow G_c(s) = \frac{1 + 0.416s}{1 + 0.319s}$$

$T = 0.15s$

$$\Rightarrow D_{\text{Rattan}}(z) = \frac{3.436z - 2.191}{z + 0.2390}$$

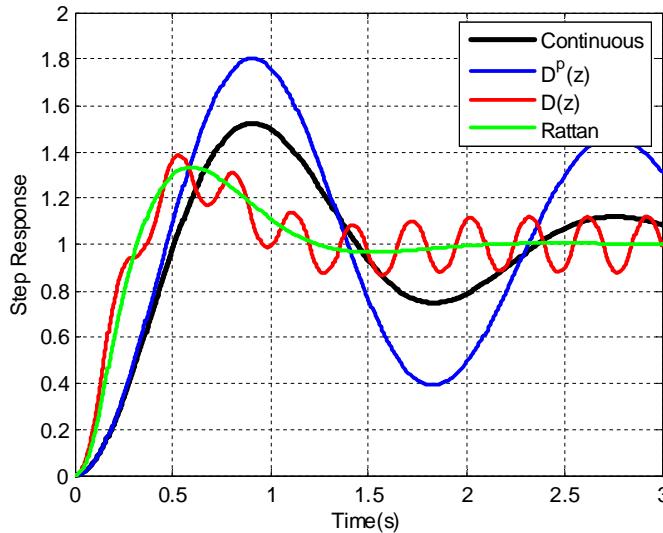
$$\Rightarrow D'(z) = \frac{2.294z - 1.5935}{z - 0.2991}$$

$$\Rightarrow D(z) = \frac{4.5888z^2 - 3.6459z + 0.3187}{z^2 + 0.5009z - 0.2393}$$

Tustin transformation

Raviv & Djaja 1999

## Examples



Raviv & Djaja 1999

## Examples

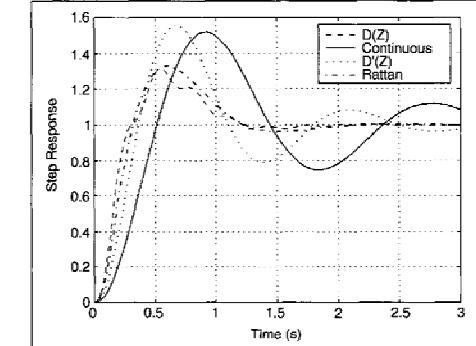
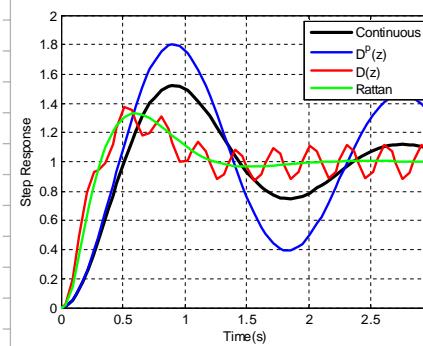


Fig. 8. Closed-loop step response of Example (d).  $T = 0.15 s$ .

Raviv & Djaja 1999

## Homework 6

- By 11pm, 5/16/09 (Sunday) by e-mail to fengli@ntu.edu.tw
- Content:
  - Homework 6 (Discretized Controller)
  - Perform your simulation study of the four examples discussed in the paper by Raviv & Djaja, 1999
  - Submit R93921XXX.m of Matlab program
    - Name, Registration Number, Department, University, etc.
    - Date:
  - Submit R93921XXX.doc of Word file
    - Name, Registration Number, Department, University, etc.
    - Date:
    - From Matlab/Figure,  
use Edit/Copy Figure to copy every figure generated by the Matlab program
    - When copying figures, set up the following options:
      - > Edit/Copy Options
        - » Clipboard format      -> Preserve information
        - » Figure background color      -> Transparent background
        - » Size      -> Match figure screen size
  - Discuss in detail how do you set up your simulation
  - Provide any possible description or explanation for each figure
  - Further discussions if possible