20.8 A 2×25Gb/s Deserializer with 2:5 DMUX for 100Gb/s Ethernet Applications

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The ever growing bandwidth requirement for novel server technologies including multi-core processing, virtualization, and networked storage leads to multichannel Internet connectivity such as 100GbE. Among the proposed standards [1], those with 4 channels (e.g., 100GBASE-ER4) are selected to arrive at a reasonable component count in discrete and photonic integration. This paper presents a 2-channel receiver prototype that amplifies, retimes, and deserializes the data in the same manner as a full 4×25Gb/s receiver, providing CMOS design examples and references for fully-integrated 100GbE transceivers.

The receiver architecture is shown in Fig. 20.8.1. Two channels process the input data independently, presenting an aggregate data rate of 50Gb/s. Each channel consists of a limiting amplifier (LA) with constant gain biasing, and a full-rate clock and data recovery (CDR) circuit. The two retimed data streams are further demultiplexed into five 10Gb/s lanes in parallel. The two 25GHz clocks distilled from the data streams are sent to a clock generator, which creates 2.5, 5, 10, and 12.5GHz clocks for the subsequent deserializer. At 25Gb/s. it is difficult to conduct 1:5 demuxing directly with reasonable power and skew, because one CDR needs to drive at least 5 flipflops simultaneously. The clock generation suffers as well since a ÷5 circuit must be made at 25GHz. Here, we perform an additional 1:2 demuxing right after the CDR to relax the stringent speed requirement. The 1:5 demuxing can therefore be realized in a relaxed way, and finally five 4:1 MUXes are incorporated to produce five 10Gb/s outputs. Note that the two channels may be subject to finite phase difference due to imbalance. A deskew circuit is placed in channel 2 to line up its 2.5Gb/s data streams with those in channel 1. This adjustment is mandatory because the middle 4:1 MUX handles inputs from both channels. A full 4×25Gb/s receiver can easily be implemented by using 2 identical chipsets proposed here.

The limiting amplifier design is illustrated in Fig. 20.8.2(a), where 5 identical gain stages are cascaded to achieve high gain (~26dB) while maintaining broad bandwidth (f_{-3dR} >42GHz). Offset is canceled by means of an *RC* feedback loop, which reveals a corner frequency of 2.5kHz. Each gain stage is realized as a simple differential pair with triple-resonance peaking [2], where the loading (150 Ω in parallel with a pMOS resistor) and the tail current are regulated by the constant-gain bias circuit, i.e., a constant loading resistance ($\approx 125\Omega$) and a constant bias current (~4mA). In other words, the small-signal gain as well as the maximum output swing (≈500mV) are fixed over temperature and process variations. The control signals $V_{\rm h,B}$ and $V_{\rm h,I}$ are generated as illustrated in Fig. 20.8.2(b). First, a sub-1V bandgap reference [3] is adopted to create a voltage of 0.7V (=1.2V – 0.5V) and a current (4mA) which are immune from PVT variations. In nano-scale CMOS, a single-deck current source is prone to channel-length modulation when mirroring. Thus, we use the loop of R_1 , Opamp 1, and M_1-M_2 to "refine" the tail current bias $(V_{b,l})$, which connects to all current sources in the gain stages. It is because R_1 (=40 Ω) suppresses the excessive V_{DS} of I_{SS} and M_2 mimics the operation of the switching pair. Note that if we were to bias the gain cells with the bandgap current directly, the mirrored current would vary by 8%. The created $V_{b,l}$ also biases M_3 , which together with M_4 and Opamp 2 forms another loop to produce $V_{\rm b,R}$. The equivalent loading resistance is determined by the desired output swing and is nominally equal to 125Ω (=500mV/4mA). Simulation suggests that both feedback loops are stable without any confliction. Using this compensation biasing, the gain and -3-dB bandwidth variations for different processes and temperatures (0°C~100°C) are reduced from 9dB to 5dB and from 25GHz to 2GHz, respectively. Supply variation can be suppressed by adopting a voltage regulator. The CDR circuit follows the design in [4]. Taking advantage of 65nm CMOS, we increase the speed by 25% while reducing the power by 33%.

The 25Gb/s 1:2 DMUX is realized as a tree structure of CML flipflops with two outputs aligned in phase [5]. The subsequent 1:5 DMUX necessitates proper

phase arrangement to assemble the 20×2.5Gb/s data. As shown in Fig. 20.8.3(a), a 5-phase 2.5GHz clock is used to sample the 12.5Gb/s incoming data sequentially. Here, the outputs need to be separated by an angle as close as 180°. Retiming flipflops driven by ϕ_3 and ϕ_5 are therefore placed to launch { D_{out1} , D_{out2} , D_{out3} } and { D_{out4} , D_{out5} } at the rising edges of ϕ_3 and ϕ_5 , respectively. A deskew circuit must be incorporated here. For example, if channel 2 data need to be aligned with phase 3 in channel 1 ($\phi_{3,CH1}$), one retiming flipflop (FF₁) is sufficient theoretically [Fig. 20.8.3(b)]. However, in practice an error may occur if channel 2 data transition is too close to the rising edge of $\phi_{3,CH1}$. To ensure proper sampling, we assign ±72° around $\phi_{3,CH1}$ as forbidden area (gray). If channel 2 data transition locates in this region, a pre-sampling is made (by FF₂) so that the data is shifted before the main sampling of $\phi_{3,CH1}$. Depending on the skew, the control logic picks Q_A or Q_B from the 2-to-1 selector. Such a design covers skew range of one complete UI (400ps).

The clock generator is shown in Fig. 20.8.4. Two 25GHz clocks from CDRs are first divided by 2 and then divided by 5. The 25GHz \div 2 circuit is realized as static topology with an inductively-peaked flipflop. The 5-phase \div 5 circuit is implemented as that in [6]. All blocks here are made of CML structures including the NAND gate. One 2.5GHz clock is sent to the 10GHz CMU (made of *LC*-tank oscillator, type IV PFD, and third-order on-chip loop filter) to create clocks for the 4:1 MUXes. The 10GHz clock synchronizes all five 10Gb/s data outputs.

The circuit has been fabricated in 65nm CMOS technology. It consumes a total power of 510mW for 2 channels, of which 32×2mW dissipates in LAs, 99×2mW in CDRs, 128mW in the 2:5 DMUX, and 120mW in the clock generator. A 1.2V supply voltage is used throughout the chip except the 2:5 DMUX, which requires a 1.4V supply to accommodate larger data swing. The input matching presents an S_{11} less than -13dB from dc to 25GHz. The CDR presents an operation range of 640MHz, across which no performance degradation is observed. Figure 20.8.5(a) and (b) depict one CDR recovered data (25Gb/s) and one final output data (10Gb/s) in response to a 2³¹-1 PRBS, revealing jitter of 1.02ps.rms/6.00ps.pp and 1.45ps,rms/8.89ps,pp, respectively. The CDR bandwidth is about 10MHz. The phase noise plots of the recovered clocks at 25GHz and 10GHz are also recorded in Fig. 20.8.5(c), suggesting -108 and -111dBc/Hz at 1MHz offset. The integrated rms jitters from 100Hz to 1GHz are 254fs and 340fs, respectively. It achieves BER<10⁻¹² for input greater than 20mV_{nn}. Figure 20.8.6(a) shows the jitter tolerance of one 10Gb/s output in response to a 100mV_{nn} 27-1 PRBS input, which exceeds the extrapolated IEEE 802.3ae mask by at least 0.27UI_{np} for all the measurable jitter frequencies (the highest allowable modulation magnitude and rate of our BERT are $160UI_{oo}$ and 10MHz, respectively). The on-chip inter-channel crosstalk is also measured. Figure 20.8.6(b) depicts the channel 1 output BER as a function of input power with channel 2 turned on and off, implying a power penalty of 1.3dB. Figure 20.8.7(a) shows the die photograph, which occupies 1.9×1.3mm². A table summarizing the receiver performance is shown in Fig. 20.8.7(b).

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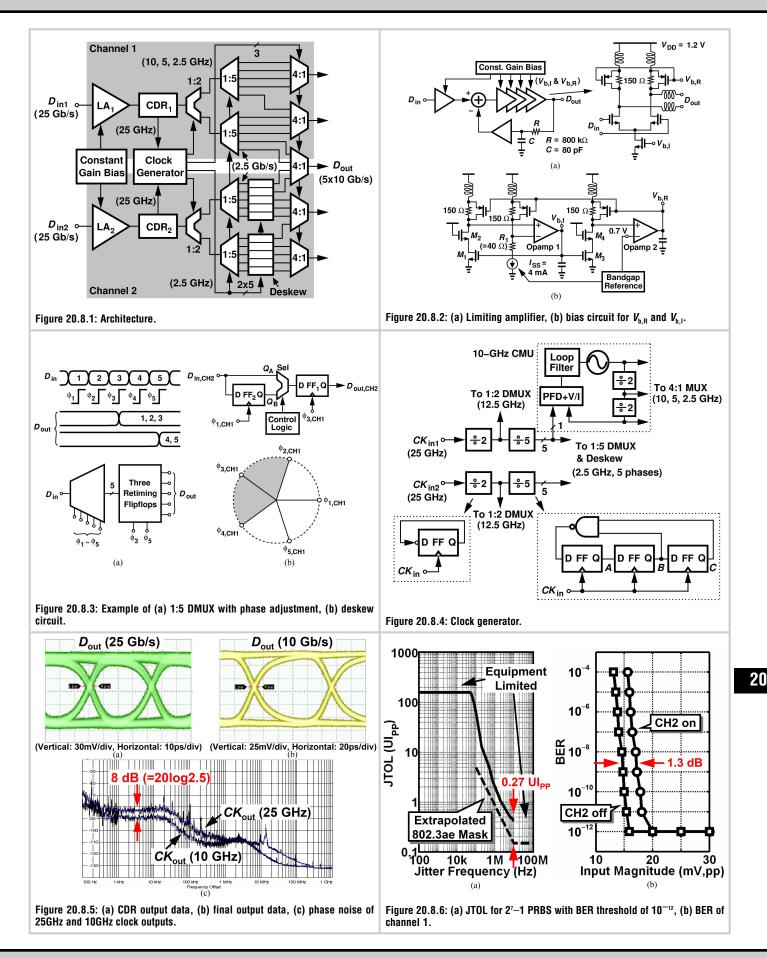
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